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Overview of the Accident in Fukushima Daiichi Nuclear Power Plant

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The Main Shock and Aftershock of the Earthquake on March 11, 2011



Earthquake Research Institute, The University of Tokyo



Tsunami after the Earthquake on March 11, 2011

Compiled by 80 members from 33 organization including The University of Tokyo http://www.coastal.jp/ttjt/

Fukushima Daiichi Nuclear Power Plants operated by TEPCO



BWR with Mark-I Type Containment Vessel (Fukushima Daiichi, Units 1,2,3,4 and 5)



Suppression Chamber (S/C)

Summary of Fukushima Daiichi Nuclear Power Plants

	Unit 1	Unit 2	Unit 3	Unit 4	Unit 5	Unit 6
	BWR-3	BWR-4	BWR-4	BWR-4	BWR-4	BWR-5
PCV Model	PCV Model Mark-I Mark-I Mark-I		Mark-I	Mark-I	Mark-II	
Electric Output	460MWe	60MWe 784MWe 784MWe 784MWe		784MWe	784MWe	1100MWe
RPV Operation Pressure	Pressure 6.89MPa 6.93MPa 6.93MPa 6.93MP		6.93MPa	6.93MPa	6.93MPa	
RPV Max. Design Pressure	8.24MPa	8.24MPa	8.24MPa	8.24MPa	8. 62MPa	8.62MPa
RPV Max. Operation Temp.	300°C	300°C	300°C	300°C	302°C	302°C
PCV Max. Design Pressure	384kPa	384kPa	384kPa	384kPa	384kPa	279kPa
PCV Max. Pressure *	427kPa	427kPa	427kPa	427kPa	427kPa	310kPa
PCV Max. Temp	140°C	140°C	140°C	140°C	138°C	171°C:D/W 105°C:S/C
Commercial Operation	1971.3.26	1974.7.18	1976.3.27	1978.10.12	1978.4.18	1979.10.24
Emergency DG	2	2 **	2	2 **	2	3 **
Electric Grid		275	500kV×2			
Plant Status on Mar. 11In Operation		In Operation	In Operation	Long Outage for Shroud Replacement	Refueling Outage	Refueling Outage

* Typical operating pressure of PCV is about 5 kPa.

** One Emergency DG is Air-Cooled **7**

Fuel Assemblies in Reactor Core and Spent Fuel Pool

Unit		2	3	4	5	6
Number of Fuel Assembly in the Core	400	548	548*	-	548	764
Number of <u>Spent</u> Fuel Assembly in the SFP	292	587	514	1,331	946	876
Number of <u>New</u> Fuel Assembly in the SFP	100	28	52	204	48	64
Water Volume (m³)	1,020	1,425	1,425	1,425	1,425	1,497
Heat Generation in Spent Fuel Pool (MW)	0.07	0.47	0.23	2.3	0.08	0.07

* including 32 MOX Fuel Assembly



Tsunami on March 11, 2011



Source: TEPCO

Tsunami on March 11, 2011

Fukushima Daiichi





Tsunami, March 11, 2011







15.5 m from the sea level

Inundation height of the Tsunami in Fukushima Daiichi was about 15 m.

Source: TEPCO

Tsunami

Fukushima Daiichi





* Based on 2002 guidelines for NPPs issued by the Nuclear Civil Engineering Committee of JSCE

Fukushima Daini



O.P.: Onahama bay construction base level



Loss of Off-site Power Supply and EDG in Units 1-4

Loss of the external power supply

Okuma 1L,2L : Breakers were broken due to the earthquake Okuma 3L : Under modification



<u>Recovery of Off-site Power Supply</u> Unit 2 on March 20, Unit 1,3,4 on March 22

One Air-Cooled DG (DG6B) survived in Units 5 & 6

Pylons damage by the earthquake caused loss of off-site power supply



* Recovery of Off-site Power Supply on March 20-21

Photographs from One of the Fukushima 50





- After the Tsunami,
 - No lighting available
 - What they can get are flashlights, batteries (some are removed from automobiles), fire trucks and some compressors
 - Very difficult to measure the major safety parameters like water level, reactor pressure, CV pressure

Radioactive Materials and Decay Power in Units 1, 2 and 3

Source Term just after the Shutdown				Dec	ay H	eat	afte	<u>r the</u>	Shut	<u>down</u>	<u> </u>		
Uni	t 1 Fuel					10							
	I-131 : 1	L.9 x 10 ¹⁸ B	q	eat		9				r l la i	Delia		
	Cs-137 : 2	2.0 x 10 ¹⁷ B	q	N He		, 8 7	Fukushima Daiichi Unit 1 Units 2 & 3						
Uni	t 2		•	cay	N S	6							
	I-131 : 2	2.7 x 10 ¹⁸ B	a	De	ier (5							
C_{s} -137 : 2.4 x 10 ¹⁷ Bg		3 on 3											
Uni	t 3		-	eac		2							
••••	I-131 : 2	2.7 x 10 ¹⁸ B	a	Ř		0		2		2		~	
	$C_{s-137} \cdot 2$	$4 \times 10^{17} \text{ B}$	9 0					5	10	15	20	25	30
			4					D	ays af	ter sl	hut-do	wn	
E	cample of I	Release Rat	te	а.		180							
	assumed ir	n a SA code		eat	_	160		Fuk	ushima) Daiichi l	Jnit 1, Ur	nits 2 & 3	
	Ba group	2.60E-04		V H	M	140							
	Ce group	4.00E-06		sca	Ś	100							
	Cs group	5.80E-02		Ď	ver	80							
	l group	6.70E-02		tor	NO	60	<u> </u>						
	La group	8.40E-07		ac		40							
	Ru group	5.40E-10		Re		20							
	Te group	3.00E-02				0		1	2	2	Δ	E	6
	Xe group	9.60E-01						́г) avs a	s Ifter a	- shut_d	s nwn	0

Unit 1 : Cooling by Isolation Condenser

Isolation Condenser (IC) for passive core cooling was operated (?) just after the emergency stop due to the earthquake **Inoperable as the Reactor Bldg. HPCI** battery was soaked PCV with water ‡⊿ \bowtie RPV Isolation Main Steam Turbine Electrical Condenser Line Generator Feedwater Line **Core Cooling** Condenser by **Isolation** Condenser Pump : Operable Ο PCV Spray Cooling System **X** : Inoperable Core Spray System Poison Standby Liquid Control System Tank 19 Source: Nuclear and Industrial Safety Agency Condensate Storage Tank

Unit 1 : Loss of Cooling



IC ? Water Injection nml [kPa] 900 1500 **Radiation** level increase Start S/C Venting 800 1000 at turbine operation bldg. 700 500 2000 -20 Reactor Water Level (mm) **Increase in PCV** Hydrogen **--600** Pressure (kPa) pressure explosion Suppression 7 **Pool Pressure Drywell Pressure** Loss of ECCS function **Reactor Pressure** Sea water injection via 300 fire extinguish line -15003/11 14:46 200 **Reactor Shut Down** Reactor Water Level (A) 3/11 15:42 -2000 **Reported High** 100 Station Black out radiation level -2500 0 3/11 0:00 3/16 0:00 3/12 0:00 3/13 0:00 3/14 0:00 3/15 0:00 ----- D/W Pressure[kPag] [kpag] լաայ 21

Water Level in RPV, Pressure in RPV and PCV (D/W & S/C) From March 11 to 16 in Unit 1

Source: Side event material on the "Fukushima Daiichi Accident and Initial Safety Measures Worldwide" in IAEA.

Hydrogen Explosion in the Operation Floor in Unit 1 - March 12, 15:36 -



Balance between Decay Heat and Heat Removal in Unit 1

Decay Heat ≫ Heat Removal

- Total decay heat before sea water injection greatly exceeds the amount of heat which reactor water and structural materials could absorb.
- All molten core moved to RPV bottom and they damaged RPV and run down to PCV.



Reactor Water Level and Core Temperature in Unit 1 - Simulation Trial by the MAAP code -



Assuming that IC lost its function by the Tsunami

18:00) after the scramreached bottom of active fuel in 4 and a half hours (around 19:30) after the scram

The core temperature started increasing when the reactor water level became lower than top of active fuel, then reached the core melting temperature.

Transition of Core Status in Unit 1 - Simulation Trial Results by the MAAP code -

Degree of fuel damage



- Melting starts from the central part of the core.
- In 16 hours after scram, most part of the core fell down to the RPV bottom.
- Although RPV is damaged in this provisional analysis, the actual damage of RPV is considered to be limited according to the temperatures presently measured around the RPV.





Comparison of simulation results and their sensitivity on input parameters from other severe accident analysis codes like MELCOR and THALES should also be made.

Summary of Simulation Results by the MAAP code in Unit 1

- All the fuels were melted and moved downwards from fuel range.
- RPV is likely to be damaged by molten core.

Before the Earthquake



Summary of Damage in Unit 1



MAAP code analysis indicates;

All fuel rods were melted and relocated to the RPV bottom. A considerable quantity of fuel dropped to the PCV bottom.

[Presumption by the record of reactor water level indicator] [Presumption by the heat balance between decay heat and heat removal] [Presumption by radioactive concentration of PCV gas] [Presumption by the radiation dose in RCW] [Evaluation of current state by temperature reading] etc.

- Currently water is injected to the RPV via the feed water piping. Temperature of the RPV bottom and the PCV is stable at less than 100 C.
- Almost all fuel dropped to the PCV bottom, is in contact with
- water, and is cooled.

Unit 3 Outline of Water Injection Systems







Source: Side event material on the "Fukushima Daiichi Accident and Initial Safety Measures Worldwide" in IAEA.

Balance between Decay Heat and Heat Removal in Units 2 & 3

- Decay heat generated in the period where water injection was interrupted exceeded the heat removal amount which reactor water and structural materials could absorb.
- It is assumed that certain amount of fuel possibly melted and moved downwards, which also lead damage RPV.



Summary of Simulation Results by the MAAP code in Units 2 and 3

- Most of fuels melted and moved to RPV bottom in the conservative scenario which assume smaller amount of water injection considering uncertainty of reactor water level indicator.
- Although some fuels were damaged, most of fuels remained in fuel range in the scenario based on measured water level with indicator.



Summary in Units 2 and 3



 <u>Although fuel was damaged and</u> <u>melted, some fuel remains at the</u> <u>core. And some fuel dropped to the</u> <u>RPV plenum or to the pedestal in the</u> <u>PCV.</u>

[Record of water level]

【Heat balance based on the amount of water injection】

【Evaluation by temperature in the RPV and the PCV】 etc.

Currently water is injected to the RPV via the feed water piping and core spray piping. Temperature at the each part of the PCV is stable at 100°C or less. Therefore, the fuel at each location is in contact with water, and is cooled.

Fuel Assemblies in Reactor Core and Spent Fuel Pool

Unit		2	3	4	5	6
Number of Fuel Assembly in the Core	400	548	548*	-	548	764
Number of <u>Spent</u> Fuel Assembly in the SFP	292	587	514	1,331	946	876
Number of <u>New</u> Fuel Assembly in the SFP	100	28	52	204	48	64
Water Volume (m³)	1,020	1,425	1,425	1,425	1,425	1,497
Heat Generation in Spent Fuel Pool (MW)	0.07	0.47	0.23	2.3	0.08	0.07

* including 32 MOX Fuel Assembly

Hydrogen Explosion in Unit 4 on March 15

Possible mechanisms ; (1) Zr-H₂O reaction in the SFP, (2) H₂ from Unit 3, (3) Decomposition of H₂O into H₂ and O₂ under radiation



Unit 4 : Spent Fuel Pool

No significant damage was identified by underwater camera inspection

Water sampling also shows relatively low radioactivity in SFP water

Analysis result of water in the SFP of Unit 4 (Date of Collection April 12 and 28)

Detected	Density (Bq/cm ³)	Density (Bq/cm ³)		
Nuclides	on April 12	on April 28		
Cesium 134	88	-		
Cesium 137	93	55		
Iodine 131	220	27		

Source: TEPCO



Source: TEPCO

X Zr-H₂O reaction in the SFP at high temperature
High Concentration of Hydrogen Gas Production in Water at Boiling Temperature under Radiation

G-values	-H ₂ O	e⁻ _{aq}	ОН	Н	H_2O_2	H ₂	HO ₂
Gamma-ray	4.1	2.7	2.8	0.56	0.68	0.45	~0.01
Alpha-ray	2.65	0.06	0.24	0.21	0.985	1.3	0.22

May 16, 2011 Prof. Katsumura Group



Typical BWR condition simulation of radiation chemistry reactions considering the reaction between H_2 and OH, resulting in steady state concentration of H_2 .

The University of Tokyo and JAEA

<u>New Finding by H₂ production under irradiation;</u>
➢ Effective transfer of H₂ into gas phase at 100 C
➢ High concentration of H₂ through condensation of H₂O at lower temperature region



Stand-by Gas Treatment Systems for Units 3 and 4



Pipes of stand-by gas treatment systems for Units 3 and 4 are connected. The the test of the test of the test of the test of t

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Source: TEPCO

Possible Mechanism of Hydrogen Explosion in Unit 4



On-site Radiation Monitoring in Fukushima Daiichi Site From March 11 to 18



20:50 2km Evacuation (Fukushima Pref.) 21:23 3km Evacuation & 3-10 km Sheltering in House

<u>International Nuclear Event S</u> cale (INES)					
7	<i>Off-site Impact</i> Major release	On-site Impact	Defense-in-depth Degradation		
6	Significant release				
5	Limited release	Severe damage			
4	Minor release	Significant damage / Fatal exposure of worker			
3	Very small release	Severe spread of contamination / health effects to worker	Near accident		
2		Significant spread of contamination	Significant failure		
1		/ overexposure of worker	Beyond Operation limit		
0					

Out of scale

Amount of Released Radioactive Material to determine INES Rating

INES level 7 : > 10¹⁶Bq equivalent

	Estimated release from Fukushima Daiichi				(Reference)		
	by NISA	by Nuclear Safety Commission		Release from Chernobyl			
lodine 131 (a)	130 thousands T Bq (1.3X10 ¹⁷ Bq)	150 thousands T Bq (1.5X10 ¹⁷ Bq)		1,800 thousands T Bq (1.8X10 ¹⁸ Bq)			
Cesium 137	6 thousands T Bq (6.0X10 ¹⁵ Bq)	Example of Release		sands T Bq (10 ¹⁶ Bq)		sands T Bq <10 ¹⁶ Bq)	
lodine value	line value 240 thousands T Bq		Ba group	<u>1 a sa</u> 2 a	60E-04 00E-06		ousands T Bq
conversion (b)	(2.4X10 ¹⁷ Bq)		Ce group 4 (⟨10¹8Bq)
(2) + (b)	370 thousands T Bq		Cs group	5.8	80E-02		usands T Bq
(a) + (b)	(3.7X10 ¹⁷ Bq)		l group	6.7	0E-02		(10 ¹⁸ Bq)
			La group	8.4	OE-07		
INES Manual (2008) co-sponsored by IAE.			Ru group	5.4	0E-10		
			Te group	3.0	0E-02		
			Xe group	9.6	60E-01		

On-site Radiation Monitoring in Fukushima Daiichi Site From March 11 to April 10



On-site Radiation Monitoring in Fukushima Daiichi Site From March 11 to October 17

dose rate measured at on-site monitoring posts



Monitoring Radiation Dose in Fukushima Prefecture



Date and Time

Source: MEXT press release



Radiation Monitoring at The University of Tokyo

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Tokyo, Hongo Campus : 230 km

Integrated Dose by External Exposure



SPEEDI code

Adult

from March 12 to April 24, 2011

Effective Dose in mSv

:	100	
Ξ	50	
Ξ	10	
:	5	
:	1	



Cesium Deposition

April 29, 2011

20 k

Evacuation of Residents



- 230 km from Tokyo
- 580 km from Osaka
- 600 km from Sapporo

Evacuation of Residents

The government took measures such as taking shelters or evacuation as follows based on the reports from Fukushima Daiichi & Daini.

Fri, 11 March

- 14:46 The Earthquake
- 19:03 Emergency Declaration by the Gov't (Daiichi)
- 21:23 <u>3 km radius evacuation (Daiichi)</u> 10 km radius taking shelter (Daiichi)

Sat, 12 March

- 5:44 10 km radius evacuation (Daiichi)
- 7:45 3 km radius evacuation (Daini) 10 km radius taking shelter (Daini)
- 17:39 10 km radius evacuation (Daini)
- 18:25 20 km radius evacuation (Daiichi)

Tue, 15 March

11:00 20-30 km radius taking shelter (Daiichi)

Thu, 21 April

11:00 20 km radius is designated as "Restricted Area" (Daiichi)

Fri, 22 April

9:44 20-30 km radius taking shelter has been lifted (Daiichi)

Establishment of "Planned Evacuation Area" and "Emergency Preparation Area"



Short-term Issues

> Core cooling : Stable Cooling to Cold Shut-down by Dec. 16 ?

- Continuous and stable core cooling
- Understanding of core condition

> Mitigation

- Consideration of full-fledged processing facilities
- Safe storage of secondary wastes
- Prevention of contamination of groundwater

> Monitoring / Decontamination

- Clear understanding of contamination and release rate
- Dose reduction and decontamination

> Environmental improvement

- Dose control for workers

TEPCO's Roadmap on April 17

	Step 1 (About 3 Months)	Step 2 (Minimum about 6 to 9 Months)
Target	Steady Reduction of Radiation Dose	Controlling Radiation Release and Significant Reduction of Radiation Dose
Reactors	Stable Cooling (Water Filling over the Fuel)	Achieving the State of Cold Shutdown
Spent Fuel Pools	Stable Cooling	Keeping the Sufficient Water Level for More Stable Cooling (Remote Operation)
Radioactive Contaminated Water	Prevention of Outflow to the out of the Site	Processing and Decreasing the Contaminated Water
Radioactive Contaminated Atmosphere/Soil	Prevention of Spread	Covering Up the Entire Reactor Building 52

Major Countermeasures in the Power Station as of June 17





Measure to shield groundwater

Radiation Control for Workers

Radiation Dose from External and Internal Exposure for Workers in Fukushima Daiichi Nuclear Power Station

3,695 Workers (working from March) and 3,388 Workers (from April) * have been inspected by July 29, 2011

Radiation Dose (External + Internal): Number of Workers

100mSv~150mSv	: 86
150mSv~200mSv	: 14
200mSv~250mSv	: 2
250mSv~	: 6 (309mSv~ 678mSv)

Measures to control dose

- Information sharing : Each group of emergency response organization share the information that they have with each other and confirm judgments or directions from several points of view.
- Logistic enhancement : Deploy necessary materials such as masks or potassium iodine so that workers can use immediately in case abnormal status of nuclear plants are predicted.
- Eating restriction : Establish eating/resting time and location. Eating shall be prohibited not only in main control rooms of Units 1~4 in Fukushima Daiichi but also in statutory radiation controlled area (per surface contamination and radioactive density in the air), etc.

Long-term Issues

Long-term storage and disposal of radioactive wastes

- Interim storage of core debris and radioactive wastes
- Final disposal of radioactive wastes

> Defueling

- Defueling from SFPs

1) Preservation of integrity of the SFP structures until completion of defueling activities

2) Construction of Fuel / Cask handling equipments

- Defueling from RPV/PCVs

1) Understanding of core condition

2) Stopping RPV/ PCV water leakage for reflooding

Decontamination

- Contaminated soil and off-site radiological mitigation
- Interim storage of primary and secondary wastes generated from decontamination work

> Decommissioning

- Handling of severely damaged and radiated core materials
- Completion of water processing

Materials Issues to be Evaluated

Evaluation of RPV/PCV materials

- Corrosion Evaluation

Proper assumption of progression of corrosion

- Mechanical Property Evaluation

Elevated temperature history exceeding design basis was observed during the accident

 \rightarrow Change in mechanical property should be evaluated for seismic analysis

RPV Pedestal

Evaluation of stability of RC (Reinforced Concrete) structure of RPV pedestal after the high temperature history and immersion to the sea water

Development of Corrosion Mitigation Techniques such as:

- Reduction of O₂ and Cl⁻
- Cathodic Protection
- Inhibitors



Erosion of Concrete in RCV in Unit 1

- Possibly the melted fuel eroded concrete at the PCV bottom. The erosion depth analysis was carried out by MAAP code. On realistic conditions, the result of the erosion depth analysis became about 0.7m.
- The gas emitted by the disassembly of concrete is not detected, indicating no further erosion of concrete by the melted fuel.



Current Schedule of Corrosion Management



Reduction of Dissolved Oxygen (Nitrogen Bubbling)



Hydrazine injection is also applied to the fuel pool of Units 2~4

Reduction of Dissolved Oxygen (Hydrazine Injection)

Hydrazine (N₂H₄) ∶

- Common deoxidant for general boilers including fossil power plants
- Also used as deoxidant in PWRs

Deoxygenation reaction by hydrazine:

 $N_2H_4 + O_2 \rightarrow N_2 + H_2O$ Reaction products (N₂, H₂O) have no negative effect on corrosion

However, hydrogen is produced by thermal decomposition reaction in >350°C range $2N_2H_4 \rightarrow 2NH_3 + N_2 + H_2$



- Hydrazine injection is applied to fuel pools where temperature is now well controlled.
- Application to RPV/PCV will be considered when the fuel cooling will be stable enough not to exceed H_2 -generation temperature.

Desalting from Spent Fuel Pools

Objective:

To reduce Cl⁻ concentration to < 10 ppm in order to prevent localized corrosion of fuel pool liner made of 304 stainless steel

System Composition:

(1) Pre-processing: Removal of oil and radioactive materials to protect RO

- (2) Reverse Osmosis membrane (RO): Transferring salt to waste liquid
- (3) Electrodialytic Treatment (ED): Condensing waste liquid

 \rightarrow Desalted water: 94%, Waste liquid: 6%



System application to SFP of Unit-4

Desalting System is mounted on trucks and will be transferred to Units 2 and 3 in series









Stability Assessment of RPV/PCV

Function as the boundary of radioactive material has been lost, however, it is still crucial until the fuel removal to:

- Secure seismic stability
- Prevent drastic increase in leak rate of coolant

Minimizing corrosion of structural materials is the key issue

Different characteristics from SFP evaluation

- Lower corrosion rate compare to localized corrosion of stainless steels More extensive consideration can be (and needed to be) performed
- Garnering information is far more difficult due to radiation-related impediments

Coordination and cooperation with another projects and institutes are important

Preliminary Lessons Learned

The importance of <u>Defense in Depth</u> has been recognized with this accident

(1) Appropriate Design Basis Accidents (DBAs)

Appropriate consideration for natural hazards by design

- Design basis tsunami height 5.7m against 15m of actual tsunami height

(2) Robustness and Diversity in Responding to beyond DBAs such as Station Black-out for Long-Duration, Loss of Ultimate Heat Sink

- ① Appropriate design philosophy to sustain safety function against common cause failures brought by natural hazards
 - All the emergency DGs, except 1 air-cooled DG, were water-cooled and all were located in the basement of T/Bs
 - All the sea-water pumps were located slightly above the design tsunami height and they were with no protection against water.
- **(2)** <u>Appropriate Accident Management (AM) measures for both prevention and</u> <u>mitigation of Severe Accidents</u>
 - No AMs for SFP cooling and Hydrogen gas control in the R/Bs
 - No AMs training under severe conditions for multi-units under continuous aftershocks

Defense-in-depth for Systems Safety

1	Prevention of Abnormal Operation and Failures	Conservative Design, High Quality in Construction and Operation
2	Control of Abnormal Operation and Detection of Failures	Control, Limiting and Protection Systems, and other Surveillance Features
3	Control of Accidents within the Design Basis	Engineering Safety Features and Accident Procedures
4 N	Control of Severe Plant Conditions including Prevention of Accident Progression and litigation of the Severe Accident Consequences	Complementary Measures and Accident Management
5 .	Mitigation of Radiological Consequences of Significant Releases of Radioactive Materials	Off-site Emergency Response

Preliminary Lessons Learned (continued)

(3) Difficult Situations for Post Severe Accident Recovery

- Warning for aftershocks and subsequent Tsunami
- High radiation in the working area
- Massive radioactive debris within the site

(4) Emergency Preparedness and Responses

- Evacuation zones
- Function of off-site center
- Communication
- Radiation monitoring

Nuclear Power Plants in Japan

2F : Fukushima Daini 1600 BWR : 26 units BWR (Permanent Shut-down) : 6 units PWR : 24 units ▲ GCR, ATR (Permanent Shut-down) 1400 Electrical Output (MWe) 1200 2F-1 2F-3 2F-2 2F-4 1F-6 1000 800 -3 1F-4 1F-2 1F1F-5 600 1F-1 400 200 0 1965 1970 1975 1980 1985 1990 1995 2000 2005 2010

Start Year of Operation

1F : Fukushima Daiichi

<u>Regulatory Systems</u> for Inspection, Periodic Safety Review and Ageing Management Technical Evaluation



Current Status of Nuclear Power Plants in Japan



Status of Nuclear Power Plants in Japan

No Restart from Regular Outage after March 11



Thank you very much.